

# Isogeometric Analysis

*The better alternative to FEM?*

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# Aim of this lunch lecture

- Give a brief introduction to Isogeometric Analysis
- Outline advantages of IgA over the Finite Element Method
- Address practical transformation of a FEM into an IgA code

# The Finite Element Method

## Strong problem formulation

Find  $u$  such that

$$Lu = f \quad \text{in } \Omega, \text{ subject to BC's and IC's.}$$

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Find  $u$  such that

$$Lu = f \quad \text{in } \Omega, \text{ subject to BC's and IC's.}$$

## Variational formulation

Find  $u \in V$  such that

$$\int_{\Omega} wLu \, dx = \int_{\Omega} wf \, dx \quad \text{for all } w \in W$$

subject to BC's and IC's.

# The Finite Element Method

## Strong problem formulation

Find  $u$  such that

$$Lu = f \quad \text{in } \Omega, \text{ subject to BC's and IC's.}$$

## Discretised variational formulation

Find  $u_h \in V_h \subset V$  such that

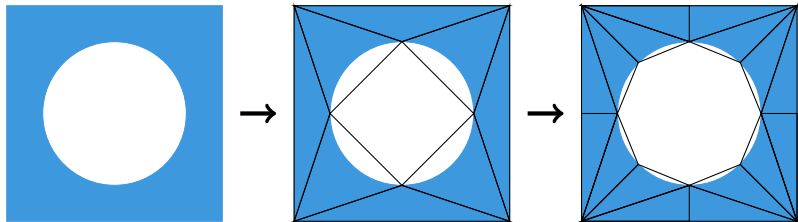
$$\int_{\Omega_h} w_h Lu_h dx = \int_{\Omega_h} w_h f dx \quad \text{for all } w_h \in W_h \subset W$$

subject to BC's and IC's.

Is  $h = \hbar$ ?

Is  $h = \mathbf{h}$ ?

**No**, since the triangulation  $\mathcal{T}_h$  of the geometry  $\Omega_h$  is in many cases of lower polynomial order (e.g., pw. linear) than the approximation of the solution  $u_h$  (e.g., pw. quadratic or higher)



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### Theoretical problem

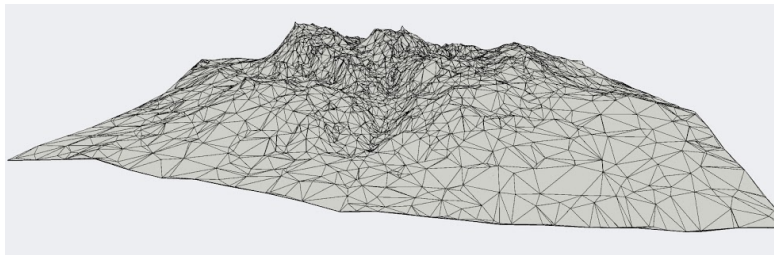
But we require computational meshes that represent the curved boundary with high accuracy to obtain optimal convergence

$$\|u - u_h\| = \mathcal{O}(h^{p+1})$$



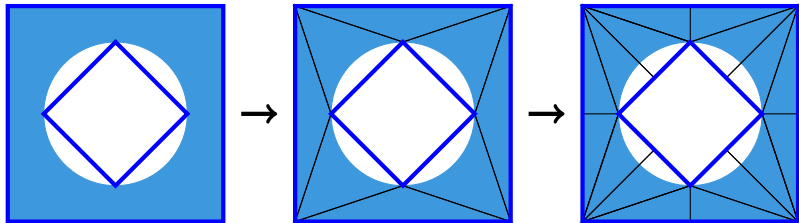
Is  $h = \mathbf{h}$ ?

**Even worse**, in many practical simulations the geometry is only given as surface triangulation  $\mathcal{S}_h$  from which the volumetric triangulation  $\mathcal{T}_h$  of the domain  $\Omega_h$  needs to be constructed



Is  $h = h$ ?

**Even worse**, in many practical simulations the geometry is only given as surface triangulation  $\mathcal{S}_h$  from which the volumetric triangulation  $\mathcal{T}_h$  of the domain  $\Omega_h$  needs to be constructed



# Common problems with the FEM

- ① How to accurately refine, coarsen and/or deform  $\Omega_h$  without a **parametric description** of the true geometry  $\Omega$ ?
- ② How to generate **high-quality curved computational meshes** for high-order methods in complex geometries?
- ③ How to define normal vectors along element boundaries?
- ④ How to construct finite element basis functions with  $C^1$  **continuity** (or higher) across element boundaries?
  - Would lead to globally continuous derivative field
  - Would solve many problems with Material Point Method

# Example

## Poisson's problem

Find  $u$  such that

$$\begin{aligned} -\Delta u &= f & \text{in } \Omega &= \{(x, y) \in \mathbb{R}^2 : x^2 + y^2 = 1\} \\ u &= 0 & \text{on } \Gamma &= \partial\Omega \end{aligned}$$

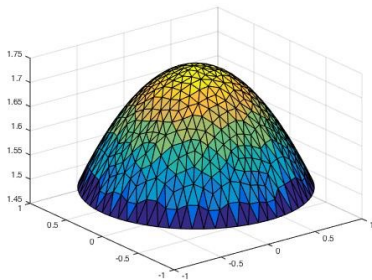
## Discretised variational formulation

Find  $u_h \in V_h = \{u_h \in \mathcal{H}^1(\Omega_h) : u_h = 0 \text{ on } \Gamma\}$  such that

$$\int_{\Omega_h} \nabla w_h \cdot \nabla u_h \, d\mathbf{x} = \int_{\Omega_h} w_h f \, d\mathbf{x} \quad \text{for all } w_h \in W_h = V_h$$

# Example

The finite element solution with **pw. linear boundary approximation** and **pw. quadratic basis functions** looks like this



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The finite element solution with **pw. linear boundary approximation** and **pw. quadratic basis functions** looks like this



# The mission

## Isogeometric Analysis

Computational analysis framework that ensures  $h = \mathbf{h}$

- Make use of a parametric description of the geometry ( $\Omega = \Omega_{\mathbf{h}}$ ) throughout all computational steps (FE-analysis, refinement/coarsening, shape deformation, multi-physics coupling, ...)
- Use the same mathematical tools (**B-splines** or NURBS or ...) to represent the geometry  $\Omega_{\mathbf{h}}$  and the FE-solution  $u_{\mathbf{h}}$

# Polynomial spaces

## Polynomial space

The space of polynomials of degree  $p$  over the interval  $[a, b]$  is

$$\Pi^p([a, b]) := \{q(x) \in C^\infty([a, b]) : q(x) = \sum_{i=0}^p c_i x^i, c_i \in \mathbb{R}\}$$

Example:  $\Pi^2([0, 1])$

- Canonical basis

$$\mathcal{B} = \{1, x, x^2\}$$

- Polynomials

$$q(x) = c_0 + c_1 x + c_2 x^2$$



# Spline space

## Polynomial splines

Let  $\mathcal{P} = \{a = x_1 < \dots < x_{p+1} = b\}$  be a partition of the interval  $\Omega_0$  and  $\mathcal{M} = \{1 \leq m_i \leq p+1\}$  a set of positive integers. The polynomial spline of degree  $p$  is defined as  $s : \Omega_0 \mapsto \mathbb{R}$  if

$$s|_{[x_i, x_{i+1}]} \in \Pi^p([x_i, x_{i+1}]), \quad i = 1, \dots, k$$

$$\frac{d^j}{dx^j} s_{i-1}(x_i) = \frac{d^j}{dx^j} s_i(x_i), \quad \begin{array}{l} i = 2, \dots, k, \\ j = 0, \dots, p - m_i \end{array}$$

Polynomial splines of degree  $p$  form the spline space  $\mathcal{S}(\Omega_0, p, \mathcal{M}, \mathcal{P})$ .

## Open knot vector

An open knot vector is a sequence of non-decreasing coordinates  $\xi_i \in [a, b] \subset \mathbb{R}$  in the parameter space  $\Omega_0 = [a, b]$

$$\Xi = (\underbrace{\xi_1 = \dots = \xi_{p+1}}_{p+1 \text{ times}}, \dots, \underbrace{\xi_i, \dots, \xi_i}_{m_i \text{ times}}, \dots, \underbrace{\xi_{n+1} = \dots = \xi_{n+p+1}}_{p+1 \text{ times}})$$

where

- $p$  is the polynomial order of the B-splines
- $n$  is the number of B-spline functions
- $\xi_i$  is the  $i$ -th knot with knot index  $i$
- $m_i$  is the multiplicity of knot  $\xi_i$

# B-spline basis functions

## Cox-de Boor recursion formula

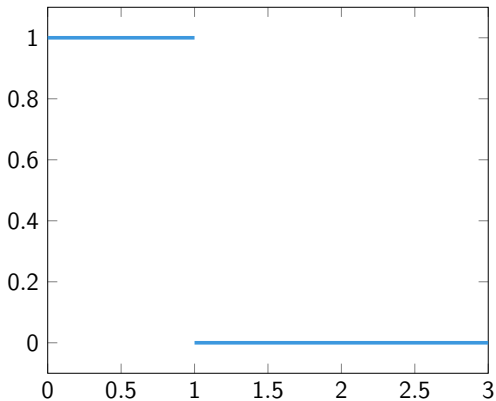
$$p = 0$$

$$N_{i,0}(\xi) = \begin{cases} 1 & \text{if } \xi_i \leq \xi < \xi_{i+1} \\ 0 & \text{otherwise} \end{cases}$$

$$p > 0$$

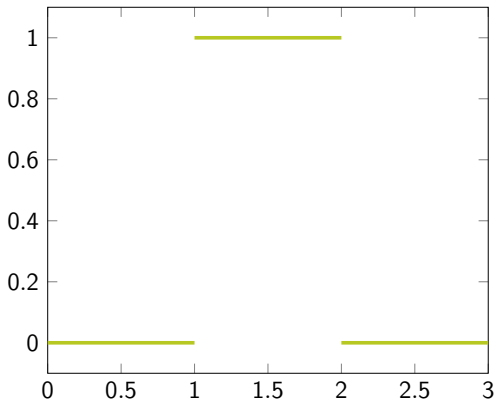
$$N_{i,p}(\xi) = \frac{\xi - \xi_i}{\xi_{i+p} - \xi_i} N_{i,p-1}(\xi) + \frac{\xi_{i+p+1} - \xi}{\xi_{i+p+1} - \xi_{i+1}} N_{i+1,p-1}(\xi)$$

# B-spline basis functions



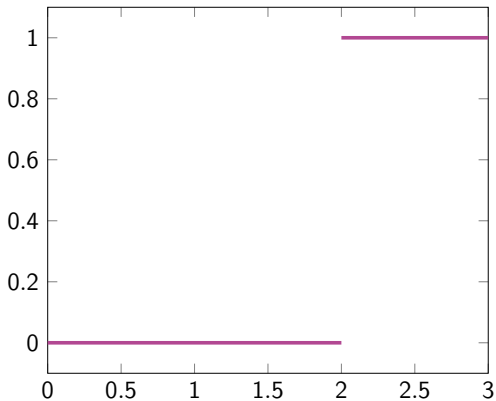
Constant basis functions corresponding to  $\Xi = \{0, 0, 0, 1, 2, 3, 3, 3\}$

# B-spline basis functions



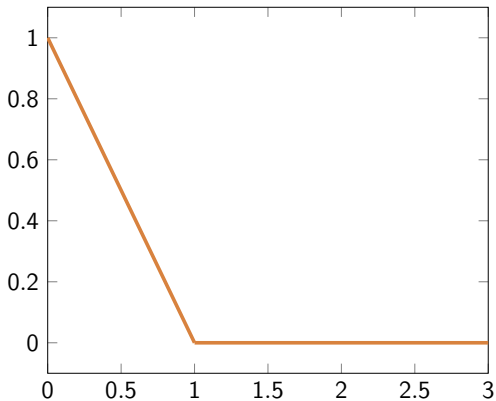
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# B-spline basis functions



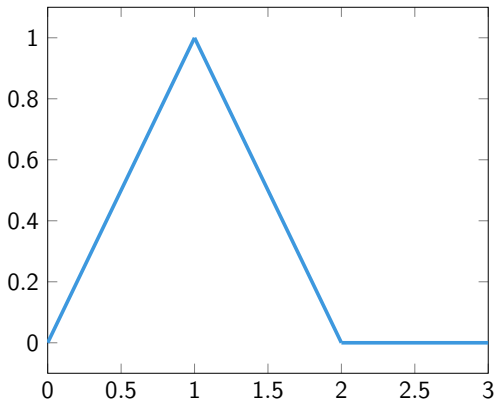
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# B-spline basis functions



Linear basis functions corresponding to  $\Xi = \{0, 0, 0, 1, 2, 3, 3, 3\}$

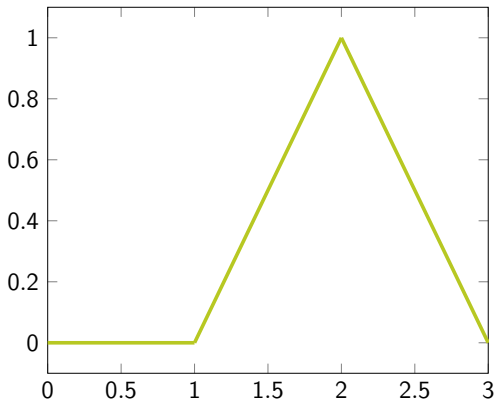
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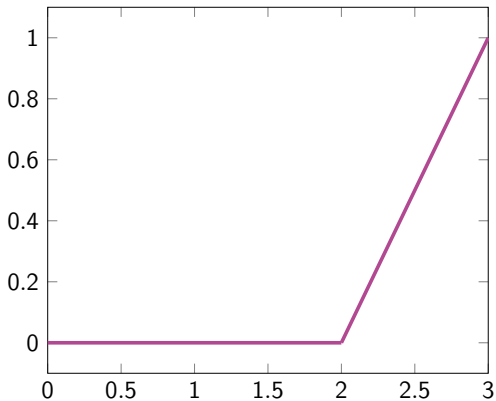


# B-spline basis functions



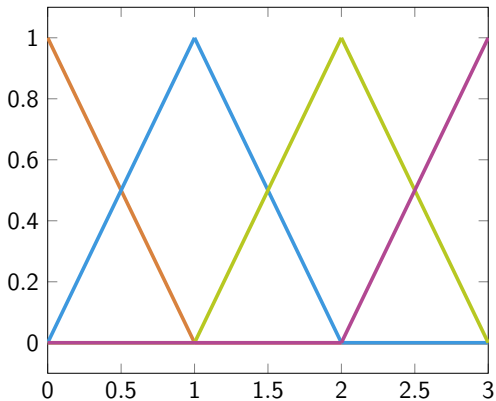
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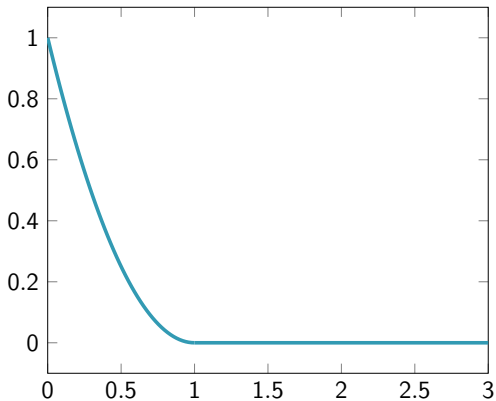
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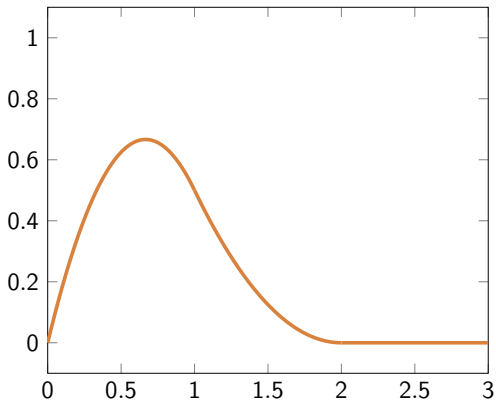
Linear basis functions corresponding to  $\Xi = \{0, 0, 0, 1, 2, 3, 3, 3\}$

# B-spline basis functions



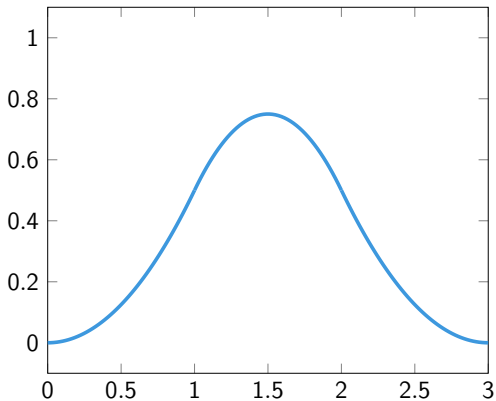
Quadratic basis functions corresponding to  $\Xi = \{0, 0, 0, 1, 2, 3, 3, 3\}$

# B-spline basis functions



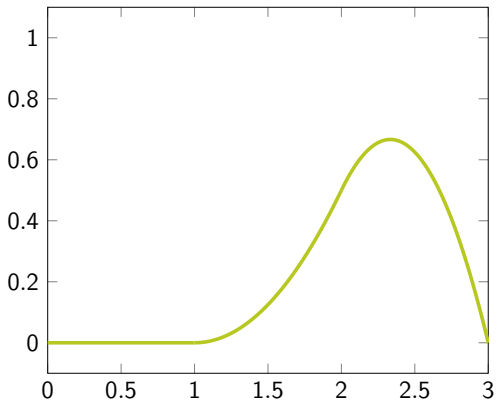
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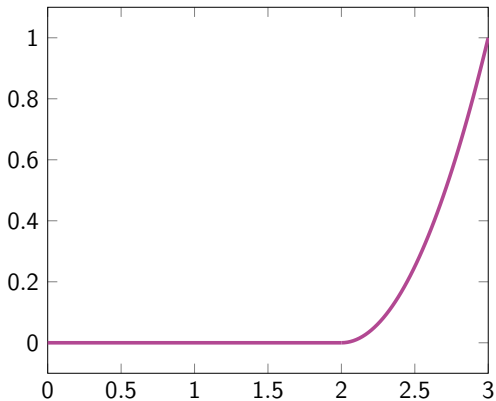
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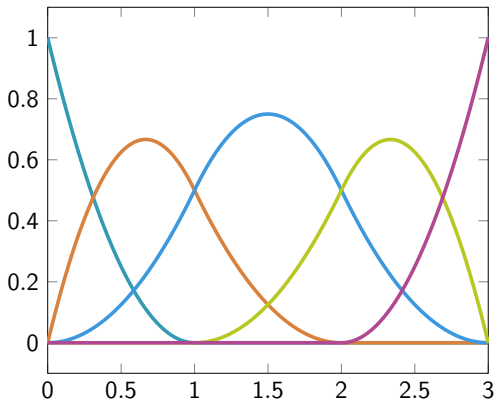
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# B-spline basis functions



Quadratic basis functions corresponding to  $\Xi = \{0, 0, 0, 1, 2, 3, 3, 3\}$

# Properties of B-spline basis functions

## Compact support

$$\text{supp } N_{i,p}(\xi) = [\xi_i, \xi_{i+p+1}), \quad i = 1, \dots, n$$

- System matrices are sparse like in the standard FEM
- Support grows with the polynomial order so that system matrices have a slightly broader stencil due to the coupling of degrees of freedom over multiple element layers

# Properties of B-spline basis functions

## Compact support

$$\text{supp } N_{i,p}(\xi) = [\xi_i, \xi_{i+p+1}), \quad i = 1, \dots, n$$

## Strict positiveness

$$N_{i,p}(\xi) > 0 \quad \text{for } \xi \in (\xi_i, \xi_{i+p+1}), \quad i = 1, \dots, n$$

- Consistent mass matrix has no negative off-diagonal entries
- Lumped mass matrix is not singular (no zero diagonal entries)

# Properties of B-spline basis functions

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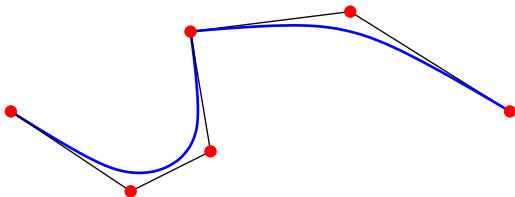
Partition of unity

$$\sum_{i=1}^n N_{i,p}(\xi) = 1 \quad \text{for all } \xi \in [a, b]$$

# Parametric geometry description

## Spline curve

$$C(\xi) = \sum_{i=1}^n N_{i,p}(\xi) \mathbf{B}_i \quad \text{set of control points } \mathbf{B}_i \in \mathbb{R}^d, d \geq 1$$

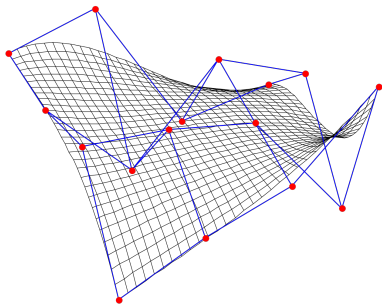


# Parametric geometry description

## Spline surface

$$S(\xi, \eta) = \sum_{i=1}^n \sum_{j=1}^m N_{i,p}(\xi) N_{j,q}(\eta) \mathbf{B}_{i,j}$$

set of control points  
 $\mathbf{B}_{i,j} \in \mathbb{R}^d, d \geq 1$



# Marriage of geometry & analysis

## Spline volume

$$V(\xi, \eta, \zeta) = \sum_{i=1}^n \sum_{j=1}^m \sum_{k=1}^l N_{i,p}(\xi) N_{j,q}(\eta) N_{k,r}(\zeta) \mathbf{B}_{i,j,k}$$

## Approximate solution

$$u_h(\xi, \eta, \zeta) = \sum_{i=1}^n \sum_{j=1}^m \sum_{k=1}^l N_{i,p}(\xi) N_{j,q}(\eta) N_{k,r}(\zeta) u_{i,j,k}$$

## Isogeometric Analysis

- 1 Construct **parametric geometry**  $\Omega(\xi, \eta, \zeta)$ :
  - generate basis  $\mathcal{B} = \{N_{i,p}N_{j,q}N_{k,r}\}_{i,j,k}^{n,m,l}$  and
  - choose control points  $\{\mathbf{B}_{i,j,k}\}$
- 2 Construct **computational mesh**  $\Omega_h(\xi, \eta, \zeta)$  and **computational basis**  $\mathcal{B}_h$  by shape preserving
  - knot insertion ( $h$ -refinement);
  - order elevation ( $p$ -refinement);
  - regularity adjustment ( $k$ -refinement)



# Application: IgA for flow problems

## Flow problems

- Convection-diffusion equation

$$\nabla \cdot (\mathbf{v}u - d\nabla u) = f$$

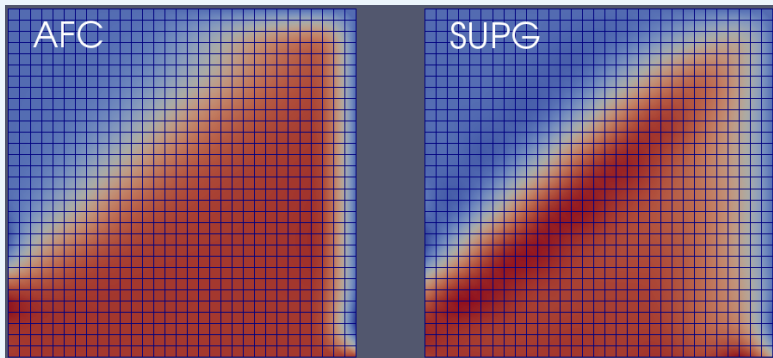
- Compressible Euler equations

$$\partial_t \begin{bmatrix} \rho \\ \rho \mathbf{v} \\ E \end{bmatrix} + \nabla \cdot \begin{bmatrix} \rho \mathbf{v} \\ \rho \mathbf{v} \otimes \mathbf{v} + \mathcal{I}p \\ \mathbf{v}(E + p) \end{bmatrix} = 0$$

Collaboration with A. Jaeschke from Technical University Łódź

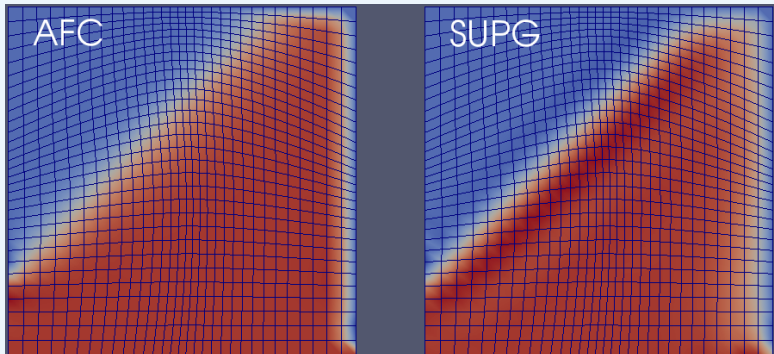
# Application: IgA for flow problems

Convection skew to the mesh



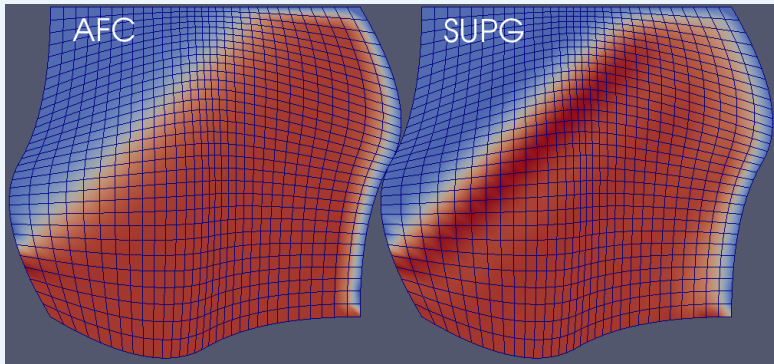
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# Application: IgA for flow problems

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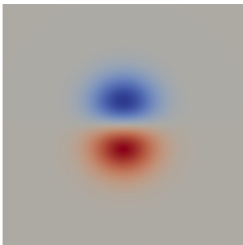


# Application: IgA for flow problems

Stationary isentropic vortex



$\rho$



$v_x$



$v_y$

- ▶ Animation: Rotation of isentropic vortex ( $\rho$ -values)

# Application: IgA on evolving manifolds

## Gray-Scott reaction-diffusion model

$$u_t + u(\ln \sqrt{g_t})_t - d_1 \Delta u = F(1 - u) - uv^2$$

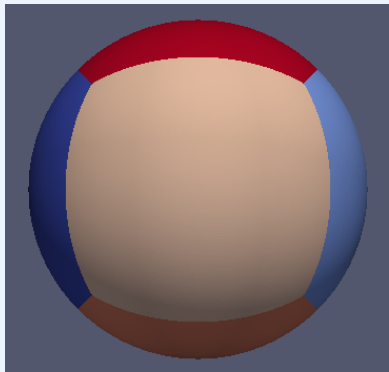
$$v_t + v(\ln \sqrt{g_t})_t - d_2 \Delta v = -(F + H)v + uv^2$$

$$\mathbf{s} = K\nu\mathbf{n}$$

MSc-thesis by J. Hinz from Technical University Delft

# Application: IgA on evolving manifolds

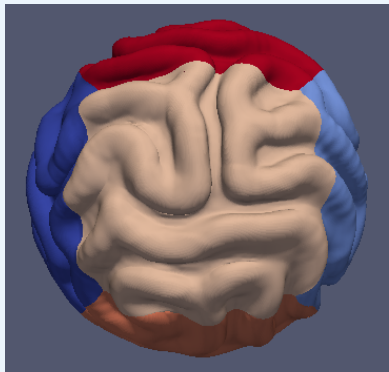
## Brain development



- multi-patch geometry
- periodic basis functions
- $C^{p-1}$  continuity along patch boundaries
- $C^0$  continuity in the vicinity of the triple points

# Application: IgA on evolving manifolds

## Brain development

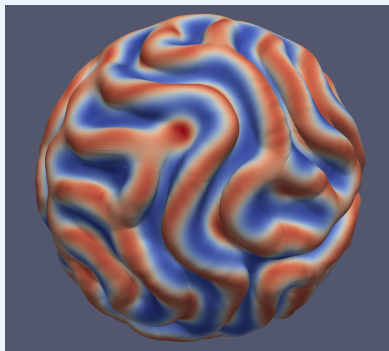


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# Application: IgA on evolving manifolds

## Brain development



- multi-patch geometry
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# Collaboration with Deltares

## Material Point Method

- Represent properties of continuum (velocity, stresses, etc.) at material points and let particles move in time
- Solve equations of motion on fixed background grid

What people like about it

- Easy treatment of free-surface, multi-phase/-material problems
- Easy treatment of large deformations (no mesh tangling)
- Easy treatment of convection (no spurious wiggles)

# Collaboration with Deltares

## Material Point Method

- Represent properties of continuum (velocity, stresses, etc.) at material points and let particles move in time
- Solve equations of motion on fixed background grid

What people 'fear' about it

- Occurrence of grid crossing errors/empty cells
- Poor convergence or even lack of convergence
- Accurate data transfer between particles and dof's in FEM
- Singularity of lumped mass matrix in higher-order FEM

# The Material Point Method

# Building blocks of MPM

Update of particle properties from dof's

$$\Delta \epsilon_p^{t+\Delta t} = \sum_{i=1}^{N_{\text{dof}}} \nabla \phi_i(x_p^t) \Delta u_i^{t+\Delta t}$$

Update of dof's from particle properties

$$\mathbf{F}_i^{\text{int},t} = \sum_{p=1}^{N_p} \sigma_p^t \nabla \phi_i(x_p^t) V_p^t$$

# IgA the better alternative to FEM?

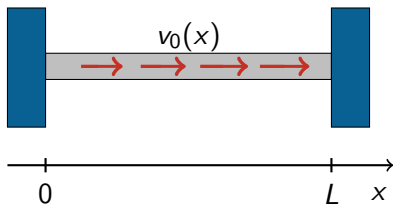
## FEM

- Lagrange-type basis functions  $\phi_i$  are  $C^0$  across element boundaries so that the values of  $\nabla\phi_i$  can have jumps
- Lumped mass matrix can become singular

## IgA

- B-spline basis functions  $N_{i,p}$  are  $C^{p-1}$  across element boundaries so that  $\nabla N_{i,p}$  is  $C^{p-2}$  (continuous for  $p \geq 2$ )
- Lumped mass matrix is non-singular

# Vibrating bar



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial x^2}$$

Boundary conditions:

$$u(0, t) = 0$$

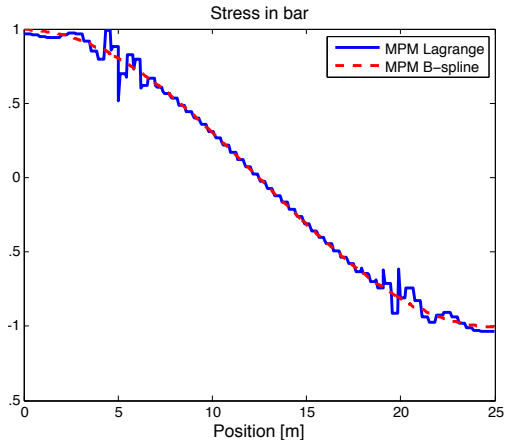
$$u(L, t) = 0$$

Initial conditions:

$$u(x, 0) = 0$$

$$\frac{\partial u}{\partial t}(x, 0) = v_0 \sin\left(\frac{\pi x}{L}\right)$$

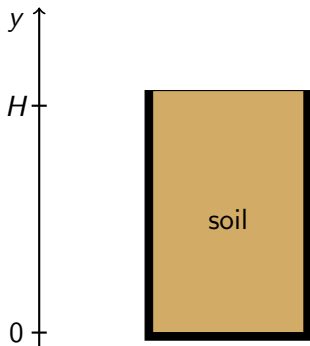
# Application: Vibrating bar



MSc-project by R. Tielen (jointly supervised with L. Beuth)



## Soil column under self weight



$$\frac{\partial^2 u}{\partial t^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial y^2} - g$$

Boundary conditions:

$$u(0, t) = 0$$

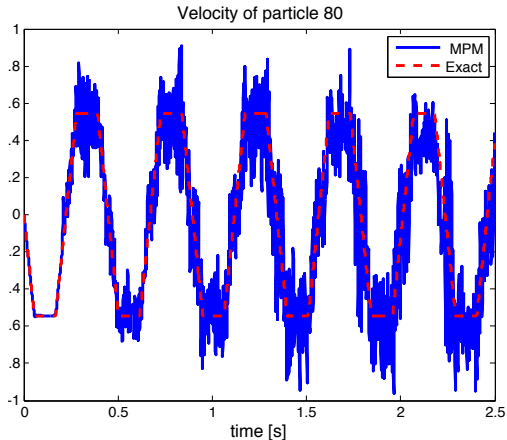
$$\frac{\partial u}{\partial y}(H, t) = 0$$

Initial conditions:

$$u(y, 0) = 0$$

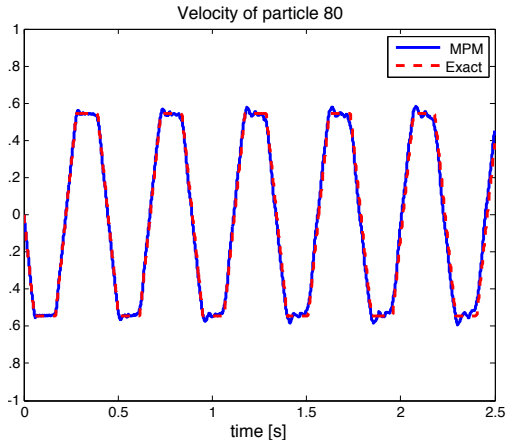
$$\frac{\partial u}{\partial t}(y, 0) = 0$$

# Application: Oedometer



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# Building blocks of your FEM code

## Finite element loop

$$A = \sum_{e \in \mathcal{T}_h} C_e K_e C_e^T$$

$$b = \sum_{e \in \mathcal{T}_h} C_e f_e$$

- Element matrix  $K_e$  and vector  $f_e$
- Connectivity matrix  $C_e$  (local-global mapping)

## Numerical quadrature

$$\int_a^b f(x) dx \approx \sum_{c=0}^N \omega_c f(x_c)$$

- Quadrature weights  $\omega_c$
- Quadrature points  $x_c$

# Building blocks of your IgA code

Loop over elements in index domain

$$A = \sum_{e=1}^{n+p} C_e K_e C_e^T$$

$$b = \sum_{e=1}^{n+p} C_e f_e$$

- Element matrix  $K_e$  and vector  $f_e$
- Connectivity matrix  $C_e$  (local-global mapping)

Numerical quadrature

$$\int_a^b f(x) dx \approx \sum_{c=1}^N \omega_c f(x_c)$$

- Quadrature weights  $\omega_c$
- Quadrature points  $x_c$

# Conclusions

- Isogeometric Analysis has several advantages over standard FEM
  - parametric geometry representation
  - no singular lumped mass matrices
  - no grid crossing errors in MPM
- Conversion of FEM code into IgA is straightforward
- Established techniques to reconstruct parametric curves, surfaces, and volumes from non-uniform sampling data
  - multi-variate spline interpolation
  - least-squares spline approximation

## List of IgA software packages

- G+SMO: [http://www.gs.jku.at/gs\\_gismo.shtml](http://www.gs.jku.at/gs_gismo.shtml)
- igatools:  
<https://github.com/igatoolsProject/igatools/wiki>
- PetIGA: <https://bitbucket.org/dalcinl/petiga/>
- GeoPDEs: <http://rafavzqz.github.io/geopdes/>
- igafem: <https://sourceforge.net/projects/cmcodes/>
- deal.II: <https://dealii.org>
- LS-DYNA: <http://www.lstc.com/products/ls-dyna>