

# the use of SIMPLE-type preconditioners in maritime CFD applications

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A horizontal banner image showing a blue ocean with white-capped waves under a clear sky.

## Overview

**Problem description:** maritime applications require large, unstructured grids

- matrix-free approach for coupled Navier-Stokes system
- only compact stencil for velocity and pressure sub-systems

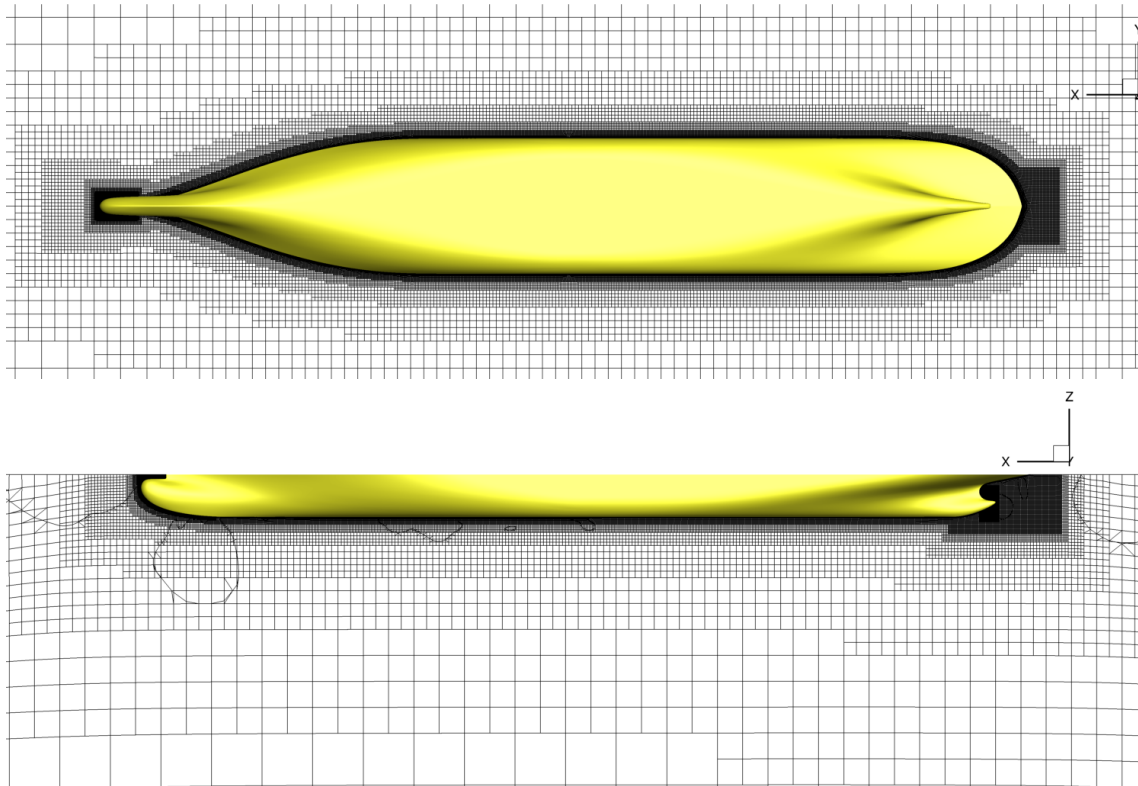
**Proposed solution:** solve coupled system with Krylov subspace method and SIMPLE-type preconditioner

- coupled matrix not needed to build preconditioner
- special treatment of stabilization

**Evaluation:** SIMPLE as solver versus SIMPLE as preconditioner

- reduction in number of non-linear iterations and wall-clock time?

## Container vessel (unstructured grid)



RaNS equations

$k$ - $\omega$  turbulence model

$y^+ \approx 1$

Model-scale:

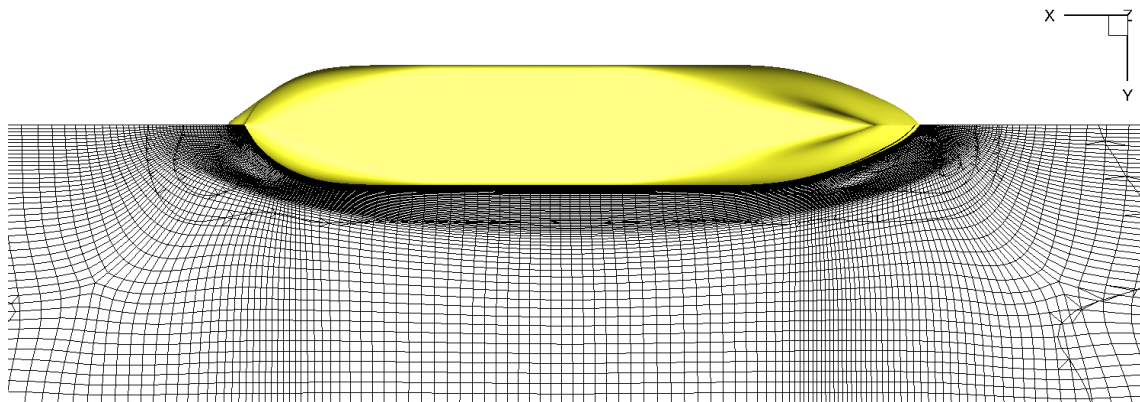
$Re = 1.3 \cdot 10^7$

13.3m cells

max aspect ratio 1 : 1600



## Tanker (block-structured grid)

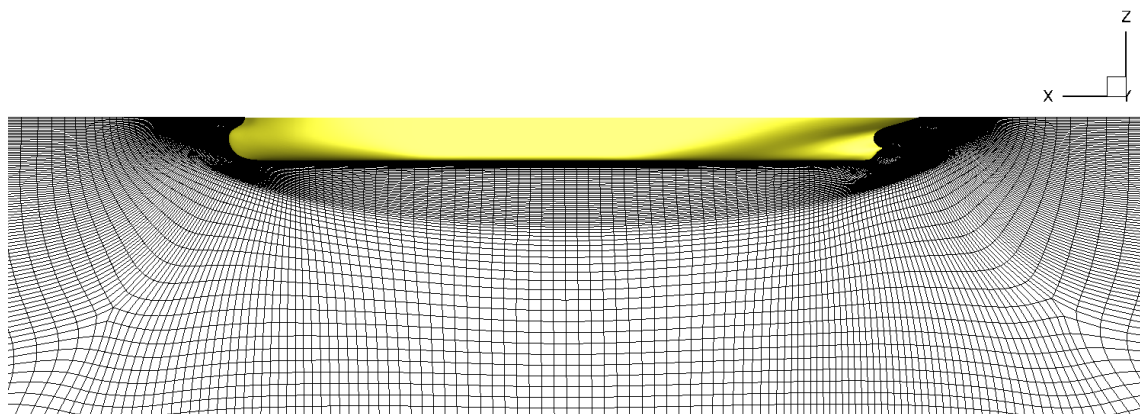


Model-scale:

$$Re = 4.6 \cdot 10^6$$

2.0m cells

max aspect ratio 1 : 7000

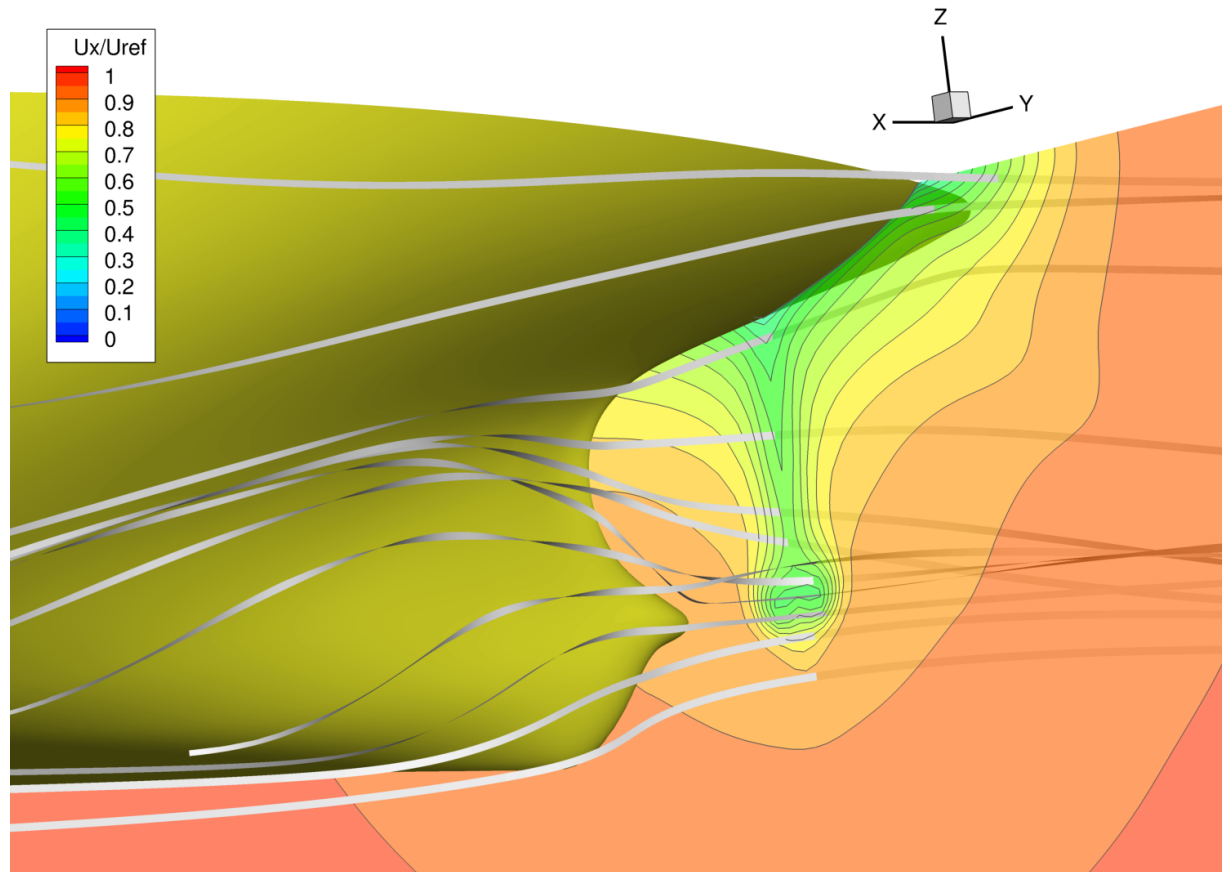
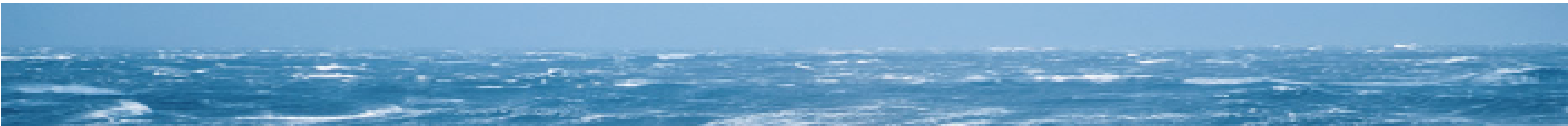


Full-scale:

$$Re = 2.0 \cdot 10^9$$

2.7m cells

max aspect ratio 1 : 930 000



streamlines around the stern and the axial velocity field in the wake.

## Discretization

Co-located, cell-centered finite volume discretization of the steady Navier-Stokes equations with Picard linearization leads to linear system:

$$\begin{bmatrix} Q_1 & 0 & 0 & G_1 \\ 0 & Q_2 & 0 & G_2 \\ 0 & 0 & Q_3 & G_3 \\ D_1 & D_2 & D_3 & C \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ p \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ g \end{bmatrix} \quad \text{for brevity:} \quad \begin{bmatrix} Q & G \\ D & C \end{bmatrix} \begin{bmatrix} u \\ p \end{bmatrix} = \begin{bmatrix} f \\ g \end{bmatrix}$$

with  $Q_1 = Q_2 = Q_3$ .

⇒ Solve system with FGMRES and SIMPLE-type preconditioner

## SIMPLE-method

Given  $u^k$  and  $p^k$ :

1. solve  $Qu^* = f - Gp^k$
2. solve  $(C - DQ^{-1}G)p' = g - Du^* - Cp^k$
3. compute  $u' = -Q^{-1}Gp'$
4. update  $u^{k+1} = u^* + u'$  and  $p^{k+1} = p^k + p'$

with approximation  $Q^{-1} \approx \text{diag}(Q)^{-1}$ .

$\Rightarrow$  “Matrix-free”: only assembly and storage of  $Q$  and  $(C - DQ^{-1}G)$ . For  $D$ ,  $G$  and  $C$  the action suffices.

## SIMPLER: additional pressure prediction

Given  $u^k$  and  $p^k$ , start with a pressure prediction:

1. solve

$$(C - D \operatorname{diag}(Q)^{-1} G) p^* = g - D u^k - D \operatorname{diag}(Q)^{-1} (f - Q u^k)$$

2. continue with SIMPLE using  $p^*$  instead of  $p^k$



## Constraints

Compact stencils are preferred on unstructured grids:

- neighbors of cell readily available; neighbors of neighbors not

Also preferred because of MPI parallel computation:

- domain decomposition, communication

Compact stencil?

✓ Matrix  $Q_1 (= Q_2 = Q_3)$

✗ Stabilization matrix  $C$

⇒ modify SIMPLE(R) such that  $C$  is not required in l.h.s.

## Treatment of stabilization matrix

- In SIMPLE, neglect  $C$  in l.h.s. of pressure correction equation

$$(C - D \text{diag}(Q)^{-1} G) p' = g - D u^* - C p^k$$

$$\Downarrow$$

$$-D \text{diag}(Q)^{-1} G p' = g - D u^* - C p^k$$

- In SIMPLER, do *not* involve the mass equation when deriving the pressure prediction  $p^*$

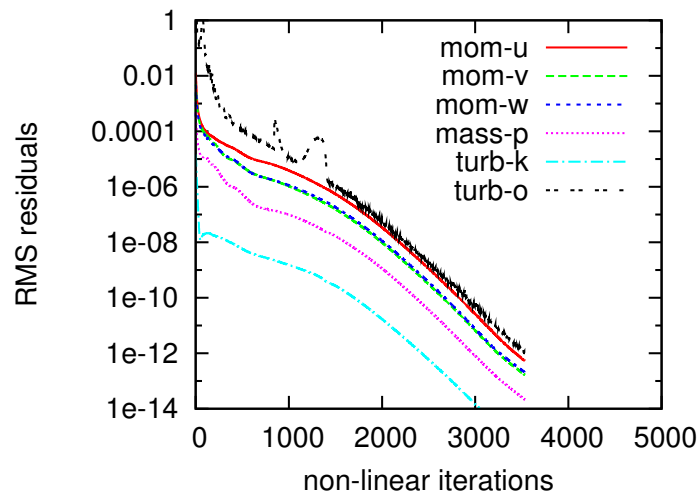
$$(C - D \text{diag}(Q)^{-1} G) p^* = g - D u^k - D \text{diag}(Q)^{-1} (f - Q u^k)$$

$$\Downarrow$$

$$-D \text{diag}(Q)^{-1} G p^* = -D \text{diag}(Q)^{-1} (f - Q u^k)$$

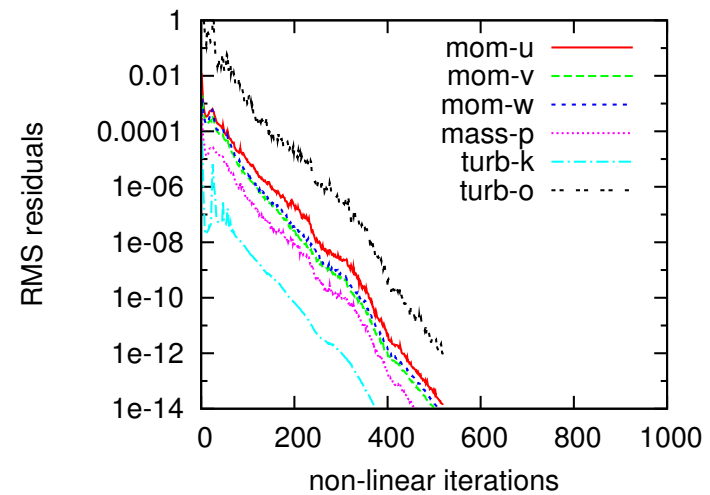
## Example of iterative convergence

SIMPLE



$$\omega_u = 0.2 \quad \omega_p = 0.1$$

KRYLOV-SIMPLER



$$\omega_u = 0.8 \quad \omega_p = 0.3$$



## Container vessel

Tables show number of non-linear iterations and wall clock time needed to converge to machine precision, starting from uniform flow.

Model-scale  $Re = 1.3 \cdot 10^7$ , max cell aspect ratio 1 : 1600

grid	CPU cores	SIMPLE		KRYLOV-SIMPLER	
		# its	Wall clock	# its	Wall clock
13.3m	128	3187	5h 26mn	427	3h 27mn

## Tanker

Model-scale  $Re = 4.6 \cdot 10^6$ , max cell aspect ratio 1 : 7000

grid	CPU cores	SIMPLE		KRYLOV-SIMPLER	
		its	Wall clock	its	Wall clock
0.25m	8	1379	25mn	316	29mn
0.5m	16	1690	37mn	271	25mn
1m	32	2442	57mn	303	35mn
2m	64	3534	1h 29mn	519	51mn

Full-scale  $Re = 2.0 \cdot 10^9$ , max cell aspect ratio 1 : 930 000

grid	CPU cores	SIMPLE		KRYLOV-SIMPLER	
		its	Wall clock	its	Wall clock
2.7m	64	29 578	16h 37mn	1330	3h 05mn

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## Summary

- Coupled Navier-Stokes system has 10 blocks, we only assemble and store 2, for the others their action suffices.
- The stabilization matrix  $C$  has a wide stencil, we changed SIMPLE(R) so that its assembly and storage is not needed.
- For maritime applications, we find that SIMPLE(R) as preconditioner reduces the number of non-linear iterations by 5 to 20 and the CPU time by 2 to 5. Greatest reduction found for most difficult case.

A wide, horizontal banner image showing a blue ocean with white-capped waves under a clear sky.

## Summary cont'd

C.M. Klaij and C. Vuik, SIMPLE-type preconditioners for cell-centered, colocated finite volume discretization of incompressible Reynolds-averaged Navier-Stokes equations, *Int. J. Numer. Meth. Fluids* (to appear), 2012.

Contains details on:

- academic benchmark cases (backward-facing step, lid-driven cavity, flat plate)
- choice of relaxation parameters
- choice of linear solvers and relative tolerances for sub-systems
- other variants (MSIMPLE and MSIMPLER)
- ...