

Finite Element Modelling Of Thermal Processes With Phase Transitions

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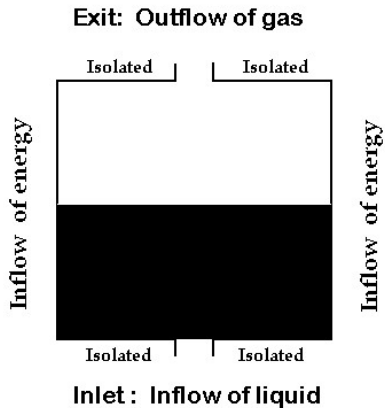


Process Industry



Security and Safety

Introduction: Boiler System



Aim and Difficulties

Aim:

Finite Element modelling of thermal processes with phase transitions using density-enthalpy phase diagrams

Difficulties:

- Nonlinearity
- Time dependent problem
- Coupled equations
- High convection: Numerical oscillations
- Accuracy and stability

Outline

- 1 Classical methods versus Density Enthalpy method
- 2 Mathematical Model
- 3 Numerical Results
- 4 2D FEM Modelling of Boiler System
- 5 Conclusions and Recommendations

Classical methods: Disadvantages

- For each phase: a set of equations
- A lot of coefficients and parameters
- Discontinuity across the interfaces
- A lot of assumptions: Less accurate

Density Enthalpy method: Advantages

- One set of equations
- Less input parameters
- Less assumptions
- Accuracy
- Stability

Density-Enthalpy phase diagrams: $T = T(\rho, h), P = P(\rho, h).$

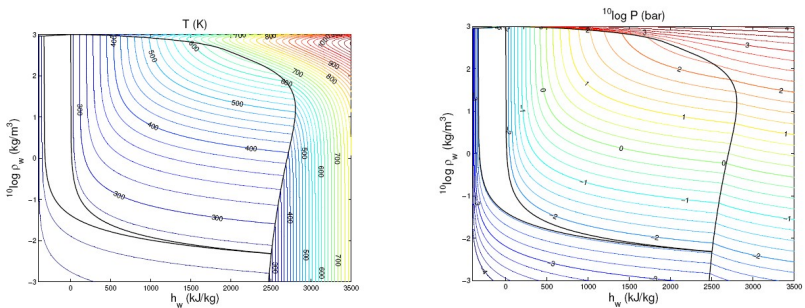


Figure: Temperature and Pressure as functions of density and enthalpy for pure water

Density-Enthalpy phase diagram: $X^G = X^G(\rho, h)$.

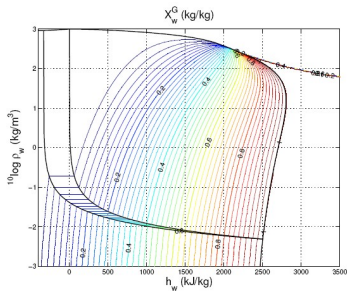


Figure: Gas Mass fraction as function of density and enthalpy for pure water

Mass and Energy balances

$$\frac{\partial \rho}{\partial t} = -\vec{\nabla} \cdot (\rho \vec{v})$$
$$\frac{\partial(\rho h)}{\partial t} = -\vec{\nabla} \cdot (\rho h \vec{v}) + \vec{\nabla} \cdot (\lambda \vec{\nabla} T) + q$$

- ρ density [Kg/m^3]
 h enthalpy [Kg/m^3]
 T temperature [K]
 \vec{v} velocity [m/s]
 λ heat conduction [$W/m/K$]
 q heat source [W/m^3]

Darcy velocity

$$\vec{v} = -\frac{K}{\mu} \vec{\nabla} P$$

- \vec{v} velocity [m/s]
- K permeability [m^2]
- μ dynamic viscosity [$Pa.s$]
- P pressure [Pa]

Boundary Conditions

The external mass transfer:

$$\rho \vec{v} \cdot \vec{n} = k_m (\rho - \rho_a)$$

k_m mass transfer coefficient [m/s]

ρ_a ambient density [Kg/m^3]

Boundary Conditions

External Energy transfer by convection:

- if $\rho - \rho_a > 0$

$$(\rho h) \vec{v} \cdot \vec{n} = h|_{\Gamma} k_m (\rho - \rho_a)$$

- if $\rho - \rho_a < 0$

$$(\rho h) \vec{v} \cdot \vec{n} = h_a k_m (\rho - \rho_a)$$

External energy transfer by conduction:

$$\lambda \vec{\nabla} T \cdot \vec{n} = k_h (T - T_a)$$

k_h heat transfer coefficient [$W/m^2/K$]

h_a ambient enthalpy [J/Kg]

Initial Conditions

$$\rho(t_0, x) = \rho_0, \quad x \in \Omega,$$

$$h(t_0, x) = h_0, \quad x \in \Omega.$$

Ω domain

t_0 starting time [s]

Numerical Approach: transform PDEs to ODEs

- Weak formulation:

$$\int_{\Omega} \frac{\partial \rho}{\partial t} \eta dV = - \int_{\Omega} \vec{\nabla} \cdot (\rho \vec{v}) \eta dV$$

- Integration by parts:

$$\int_{\Omega} \frac{\partial \rho}{\partial t} \eta dV = - \int_{\Gamma} \rho \eta \vec{v} \cdot \vec{n} dS + \int_{\Omega} \rho \vec{v} \cdot \vec{\nabla} \eta dV$$

Ω domain

Γ boundary

\vec{n} outward unit normal to $\Gamma = \partial\Omega$

η test function

Numerical Approach: transform PDEs to ODEs

- Use the boundary conditions:

$$\int_{\Omega} \frac{\partial \rho}{\partial t} \eta dV = \int_{\Gamma} \eta k_m (\rho_a - \rho) dS - \int_{\Omega} \rho \frac{K}{\mu} \vec{\nabla} P \cdot \vec{\nabla} \eta dV$$

- The solution $\rho(\vec{x}, t)$ is approximated by:

$$\rho(\vec{x}, t) = \sum_{j=0}^N \rho_j(t) \varphi_j(\vec{x})$$

ρ_j unknown density

φ_j basis function

$N + 1$ number of mesh nodes for the unknowns

Numerical Approach: transform PDEs to ODEs

- Galerkin approximation:

$$\sum_{j=0}^N \frac{d\rho_j(t)}{dt} \left(\int_{\Omega} \varphi_i \varphi_j dV \right) =$$

$$\int_{\Gamma} \varphi_i k_m \left(\rho_a - \sum_{j=0}^N \rho_j(t) \varphi_j \right) dS -$$

$$\sum_{j=0}^N \left(\int_{\Omega} \frac{K}{\mu} \vec{\nabla} P \cdot \vec{\nabla} \varphi_i \varphi_j dV \right) \rho_j(t)$$

Numerical Approach: transform PDEs to ODEs

- System of nonlinear ODEs:

$$M \frac{d\vec{\rho}}{dt} = S(\vec{\rho}, \vec{h})\vec{\rho} + \vec{F}$$

$\vec{\rho}$ unknown density

M mass Matrix

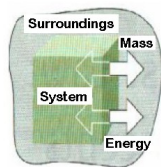
S stiffness Matrix

\vec{F} vector

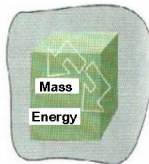
Numerical Tools

- Use SUPG method to reduce the effect of high convection,
- Use Implicit backward Euler scheme to guarantee stability.

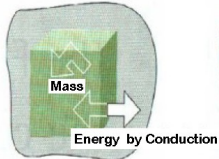
Types of simulated systems



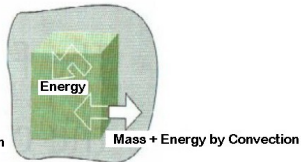
Open System



Isolated System



Closed System to Mass



Open System to Mass

Open System to Mass, $k_m = 2$, $k_h = 0$, $dt = 0.001$

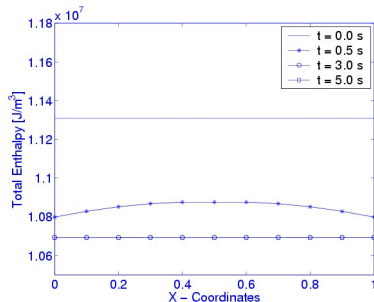
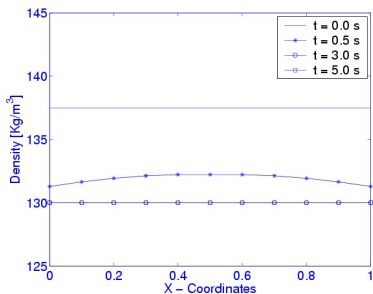


Figure: Density and Total Enthalpy after 5000 time steps

Open System to Mass, $k_m = 2$, $k_h = 0$, $dt = 0.001$

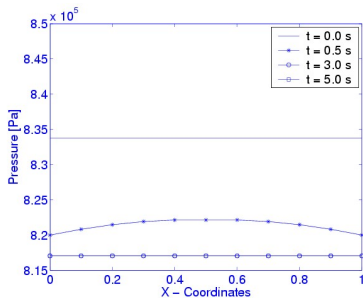
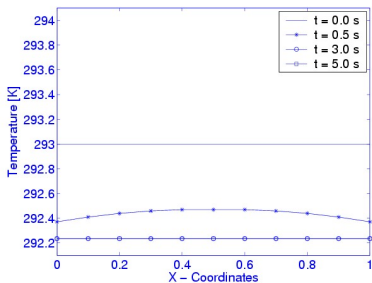


Figure: Temperature and Pressure after 5000 time steps

Open System to Mass, $k_m = 2$, $k_h = 0$, $dt = 0.001$

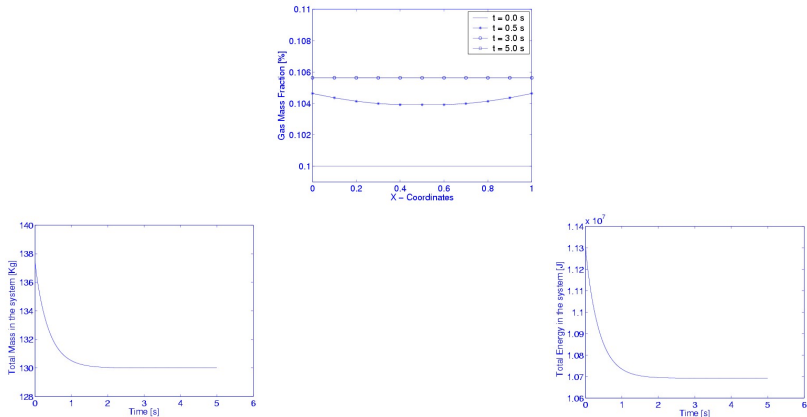


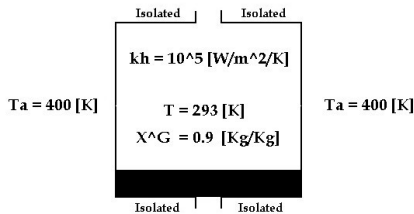
Figure: Gas Mass Fraction, Total Mass and Energy after 5000 time steps

Thermodynamical results

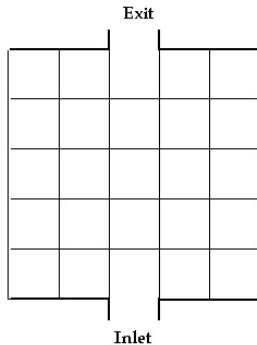
- Density inside an open system to mass, tends to the ambient density when the system reaches its steady state,
- The external transfer process of mass and energy stops as soon as the system reaches its steady state at thermodynamical equilibrium.

Geometry and Operating Conditions

Density = $18 \text{ [Kg/m}^3\text{]}$
 Enthalpy = 39.10^4 [J/Kg]
 $T_e = 393 \text{ [K]}$
 $k_{me} = 10 \text{ [m/s]}$



Density = $523 \text{ [Kg/m}^3\text{]}$
 Enthalpy = 47.10^5 [J/Kg]
 $T_i = 293 \text{ [K]}$
 $k_{mi} = 10^{-4} \text{ [m/s]}$



2D Boiler: Mass is flowing out and Energy is flowing in

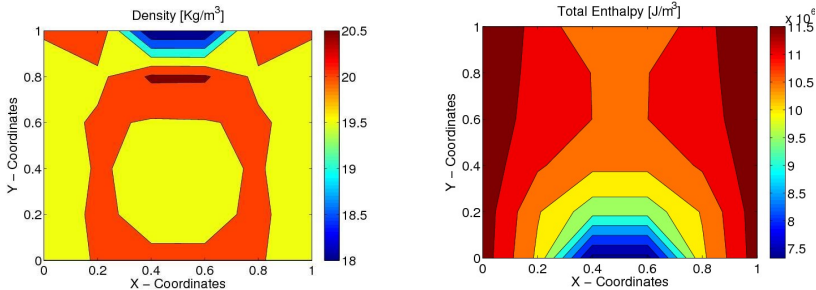


Figure: Density and Total Enthalpy with respect to x and y after 200000 time steps, $dt = 0.001$

2D Boiler: Mass is flowing out and Energy is flowing in

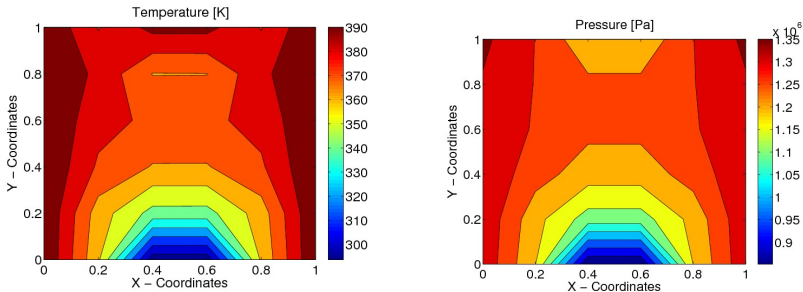


Figure: Temperature and pressure with respect to x and y after 200000 time steps, $dt = 0.001$

2D Boiler: Mass is flowing out and Energy is flowing in

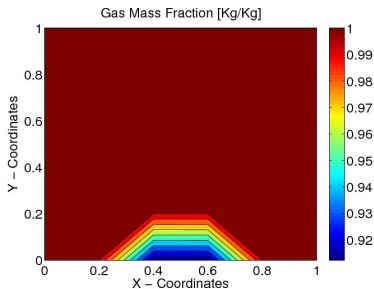


Figure: Gas Mass Fraction with respect to x and y after 200000 time steps, $dt = 0.001$

Conclusions

- 1 Set up a stable and accurate FEM model using Density-Enthalpy diagrams (0D, 1D and 2D with Matlab),
- 2 Numerical results are logical and have obtained for problems where classical methods may not work.

Recommendations

- 1 Transfer model to SEPRAN,
- 2 Study more aspects of the model (Compare implicit with explicit),
- 3 Exploit the sparsity of the matrix: essential for saving memory and computing time,
- 4 Apply iterative solvers to speed up calculations,
- 5 Validation of the numerical model: Compare with experimental results,
- 6 Add the gravity force to the equations.

Questions

