

Using CONTACT in dynamical simulations

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 - Elasticity theory
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About VORtech



- Founded in 1996 in Delft.
- Specialized in mathematical consultancy and development of high performance scientific software.
- Broad range of customers.

CONTACT

- Software that solves contact problems between two objects (e.g. train wheel & rails).
- Aims to be the worlds fastest detailed contact software.
- Originally developed by Prof.dr.ir. J.J. Kalker of TU Delft.
- Taken over by VORtech, now further developed by Dr.ir. E.A.H. Vollebregt.

Goal of this project

- CONTACT focusses on stationary problems.
- Research: how can CONTACT be used for dynamical contact problems?
- Main problem: simulation of a train over a bridge.



Elasticity theory

- Displacement $\mathbf{u}(x, y, z, t)$: Particle originally located at (x, y, z) moves to $(x, y, z) + \mathbf{u}(x, y, z, t)$.

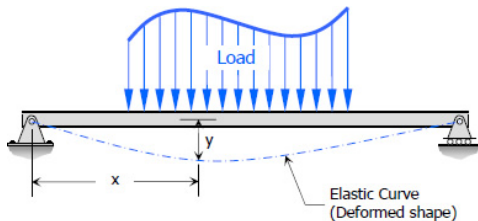


Figure: Elastic curve

The elasticity equation

$$G\Delta\mathbf{u} + (\lambda + G)\nabla(\nabla \cdot \mathbf{u}) + \mathbf{F} = \rho \frac{\partial^2 \mathbf{u}}{\partial t^2}$$

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Initial conditions:

$$u(x, y, z, 0) = u_0(x, y, z)$$
$$\frac{\partial u}{\partial t}(x, y, z, 0) = v_0(x, y, z)$$

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Example boundary conditions:

$$u(x, y, z, t) = 0 \text{ for } (x, y, z) \in \partial\Omega_1$$
$$\sigma \mathbf{n} = p \text{ for } (x, y, z) \in \partial\Omega_2$$

Contact theory

- Describes pressure distribution at the boundary of two objects.
- Different contact models:
 - ▶ Hertz model
 - ▶ Johnson-Kendall-Roberts (JKR) model
 - ▶ Derjaguin-Muller-Toporov (DMT) model
 - ▶ Maugis-Dugdale model (MD) model

Time integration schemes

General form of Newton's equation of motion

$$M(\mathbf{x})\ddot{\mathbf{x}} + P(\mathbf{x}, \dot{\mathbf{x}}) = \mathbf{F}(t)$$

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What time integration scheme should be used? Possibilities:

- Runge-Kutta / Radau methods
- Verlet method
- Newmark-Beta method

Time integration schemes

General form of Newton's equation of motion

$$M(\mathbf{x})\ddot{\mathbf{x}} + P(\mathbf{x}, \dot{\mathbf{x}}) = \mathbf{F}(t)$$

Let $\mathbf{y} = \dot{\mathbf{x}}$, so that

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{y} \\ \dot{\mathbf{y}} &= M^{-1}(\mathbf{x})(\mathbf{F}(t) - P(\mathbf{x}, \mathbf{y}))\end{aligned}\tag{1}$$

which is of the form

$$\dot{\mathbf{z}} = \mathbf{g}(t, \mathbf{z})$$

for $\mathbf{z} = \begin{pmatrix} \mathbf{x} \\ \mathbf{y} \end{pmatrix}$.

Runge-Kutta / Radau methods

All Runge-Kutta methods have the form

$$\mathbf{z}_{k+1} = \mathbf{z}_k + \sum_{i=1}^n b_i \mathbf{k}_i, \text{ where}$$

$$\mathbf{k}_i = \Delta t \mathbf{g}(t_k + c_i \Delta t, \mathbf{z}_k + \sum_{j=1}^n a_{ij} \mathbf{k}_j)$$

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c_1	a_{11}	a_{12}	\dots	a_{1n}	0	0	0	0	0
c_2	a_{21}	a_{22}	\dots	a_{2n}	$1/2$	$1/2$	0	0	0
\vdots	\vdots	\vdots	\vdots	\vdots	$1/2$	0	$1/2$	0	0
c_b	a_{n1}	a_{n2}	\dots	a_{nn}	1	0	0	1	0
	b_1	b_2	\dots	b_n		$1/6$	$1/3$	$1/3$	$1/6$

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$$\begin{array}{c|ccc}
 c_1 & a_{11} & a_{12} & a_{13} \\
 c_2 & a_{21} & a_{22} & a_{23} \\
 c_3 & a_{31} & a_{32} & a_{33} \\
 \hline
 & b_1 & b_2 & b_3
 \end{array}
 =
 \begin{array}{c|ccc}
 0 & \frac{1}{9} & \frac{-1-\sqrt{6}}{18} & \frac{-1+\sqrt{6}}{18} \\
 \frac{3}{5} - \frac{\sqrt{6}}{10} & \frac{1}{9} & \frac{11}{45} + \frac{7\sqrt{6}}{360} & \frac{11}{45} - \frac{43\sqrt{6}}{360} \\
 \frac{3}{5} + \frac{\sqrt{6}}{10} & \frac{1}{9} & \frac{11}{45} + \frac{43\sqrt{6}}{360} & \frac{11}{45} - \frac{7\sqrt{6}}{360} \\
 \hline
 & \frac{1}{9} & \frac{4}{9} + \frac{\sqrt{6}}{36} & \frac{4}{9} - \frac{\sqrt{6}}{36}
 \end{array}$$

Runge-Kutta / Radau methods

- Explicit (Runge-Kutta) methods:
 - ▶ Forward Euler
 - ▶ Runge-Kutta 4
- Implicit (Radau) methods:
 - ▶ Backward Euler
 - ▶ Radau5

The Verlet method

Applicable for problems in the form $\ddot{\mathbf{x}} = \mathbf{g}(\mathbf{x})$.

$$\mathbf{x}_1 = \mathbf{x}_0 + \mathbf{v}_0\Delta t + \frac{(\Delta t)^2}{2}\mathbf{g}(\mathbf{x}_0), \text{ and}$$
$$\mathbf{x}_{k+1} = 2\mathbf{x}_k - \mathbf{x}_{k-1} + (\Delta t)^2\mathbf{g}(\mathbf{x}_k) \quad \text{for } k \geq 1$$

Newmark's method

Implicit algorithm described by

$$\mathbf{x}_{k+1} = \mathbf{x}_k + \Delta t \mathbf{v}_k + \frac{(\Delta t)^2}{2} ((1 - 2\beta)\mathbf{a}_k + 2\beta\mathbf{a}_{k+1})$$
$$\mathbf{v}_{k+1} = \mathbf{v}_k + \Delta t ((1 - \gamma)\mathbf{a}_k + \gamma\mathbf{a}_{k+1})$$

The acceleration \mathbf{a}_{k+1} should be derived from the equations of motion:

$$M(\mathbf{x}_{k+1})\mathbf{a}_{k+1} + P(\mathbf{x}_{k+1}, \mathbf{v}_{k+1}) = \mathbf{F}(t_{k+1})$$

Contact between sphere and elastic half space

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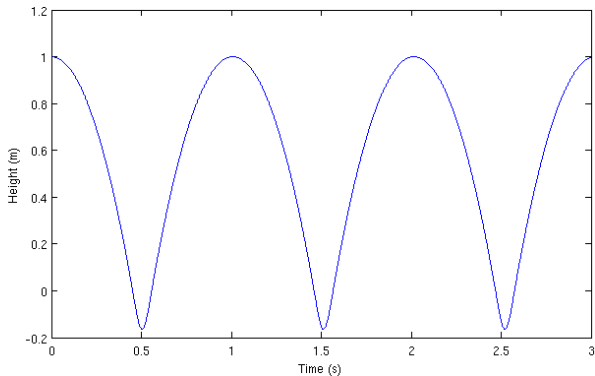
$$F_c = \frac{4}{3} E^* R^{1/2} \max(0, -z)^{3/2}$$

By Newton's second law:

$$\ddot{z} = \frac{4}{3m} E^* R^{1/2} \max(0, -z)^{3/2} - g$$

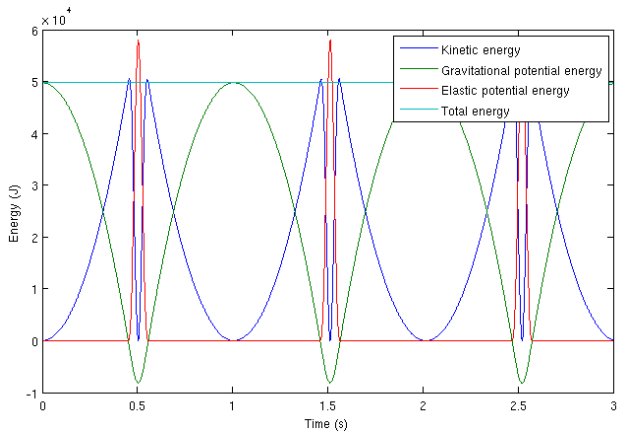
Contact between sphere and elastic half space

Using Radau5:



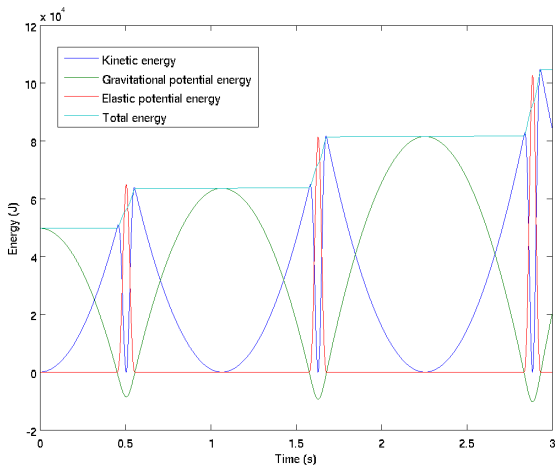
Contact between sphere and elastic half space

Using Radau5:



Contact between sphere and elastic half space

Using Forward Euler:



Deformation of a bridge

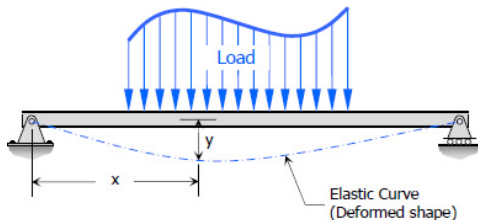


Figure: Elastic curve

Euler-Bernoulli beam equation (1D):

$$EI \frac{\partial^4 u}{\partial x^4} = -\rho \frac{\partial^2 u}{\partial t^2} + p(x, t) \quad (2)$$

$$u(0, t) = \frac{\partial u}{\partial x}(0, t) = 0 \quad (3)$$

$$u(L, t) = \frac{\partial u}{\partial x}(L, t) = 0 \quad (4)$$

Deformation of a bridge

Can be discretised using Finite Differences.

$$\frac{\partial^4}{\partial x^4} u_i(t) \approx \frac{u_{i-2}(t) - 4u_{i-1}(t) + 6u_i(t) - 4u_{i+1}(t) + u_{i+2}(t)}{\Delta x^4}$$

Results into equation

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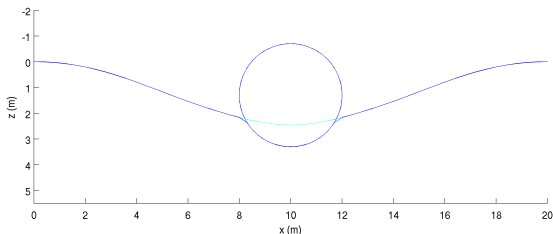
$$\ddot{\mathbf{u}} = A\mathbf{u} + p(\mathbf{u}, t)$$

Problem: CFL condition for the Verlet method:

$$\frac{EI}{\rho} \frac{\Delta t^2}{\Delta x^4} \leq \frac{1}{4}$$

Combining global and local deformations

A bridge can deform both globally and locally:



How can both phenomenons be taken into account?

Combining global and local deformations

Possibilities:

- Complete Finite Element model
 - ▶ Computationally expensive, but accurate.
- Combining the beam equation (for global deformations) and CONTACT (for local deformations).
 - ▶ Hard, since both phenomenons are not independent of each other.

Conclusion & Discussion

Literature study:

- Elasticity theory
- Contact theory & models
- Time integration methods for elastodynamics, tested on two different problems:
 - ▶ Dynamical contact between sphere and elastic half-space.
 - ▶ Global deformation of a beam.
- Implicit methods like Radau5 are preferred.

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Research:

- Research how CONTACT can be used for dynamical contact problems.
- Apply the Finite Element method.
- Long-term goal: perform train/bridge simulation, taking both global and local deformations into account.